

10.3 High-Temperature Instrumentation

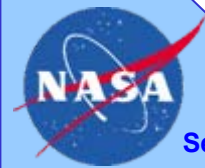
Anthony (Nino) Piazza
NASA Dryden Flight Research Center
February 28, 2008

Cleared for public release

Hypersonic Educational Initiative

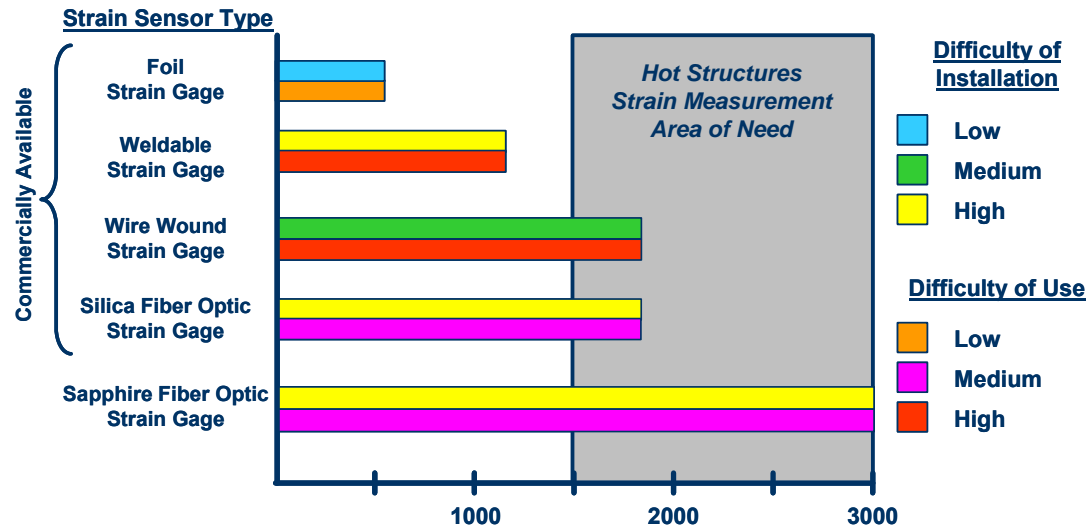
Outline

- Background
- Objective
- Application and Sensor
 - Static
 - Dynamic
- Attachment Techniques
 - Thermal Spray / Cement Applications
 - Strain Sensors
 - Thermocouples
- Evaluation / Characterization Testing
- Future Testing



Background

Sensor Development Motivation



- **Lack of Capability**

- TPS and hot structures are utilizing advanced materials that operate at temperatures that exceed our ability to measure structural performance
- Robust strain sensors that operate accurately and reliably beyond 1800°F are needed but do not exist

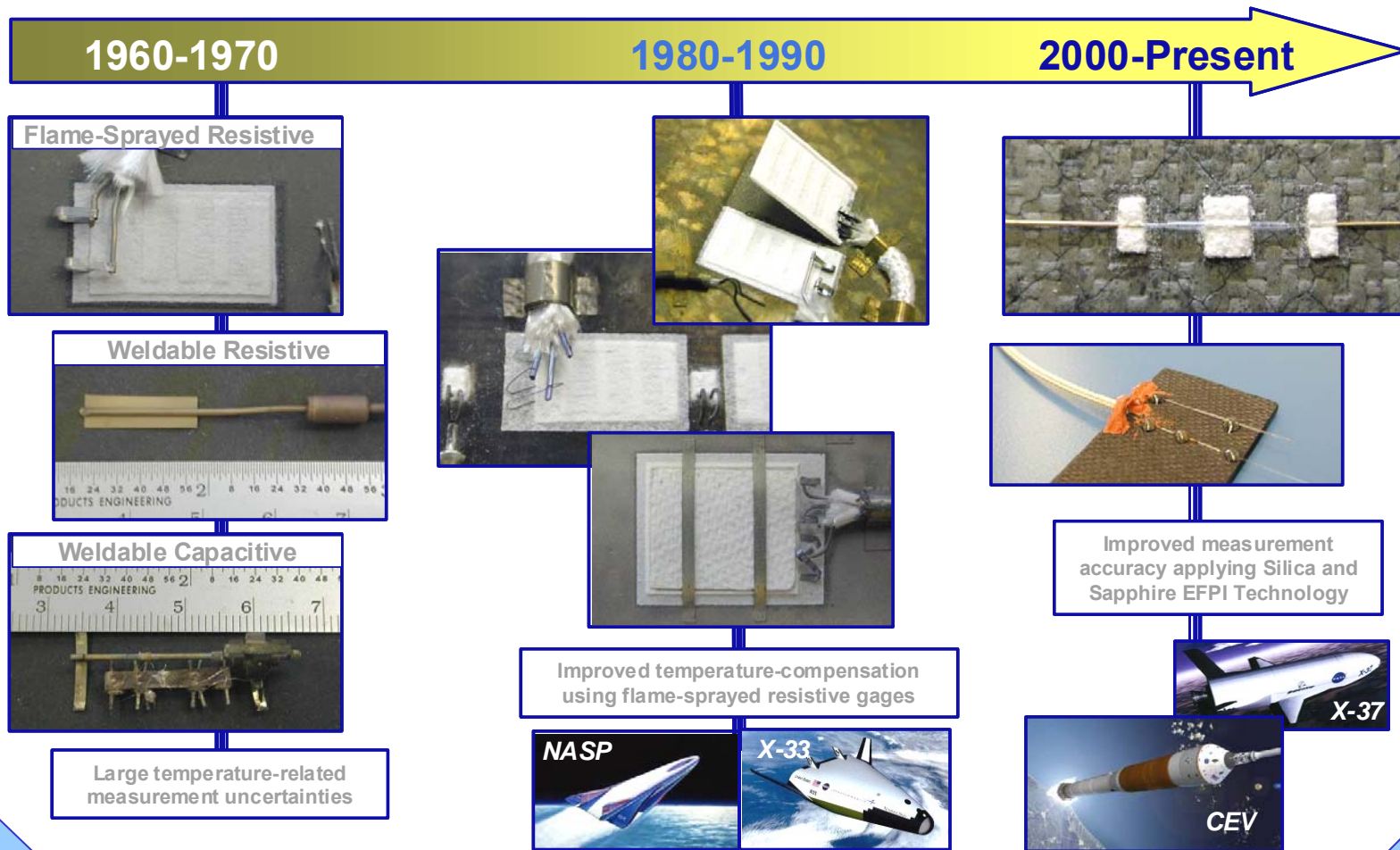
- **Implication**

- Hinders ability to validate analysis and modeling techniques
- Hinders ability to optimization structural designs



Background

Strain Sensor Maturation



Objective

Provide strain and temperature data for validating finite element models and thermal-structural analyses

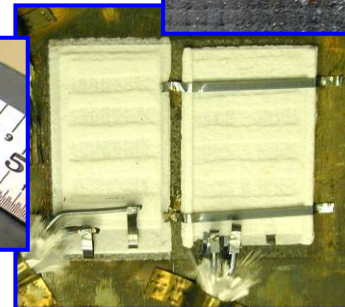
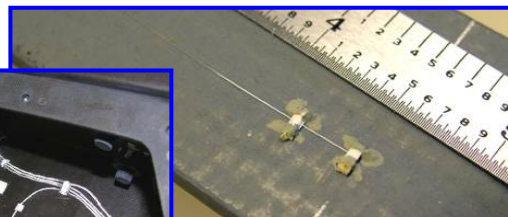
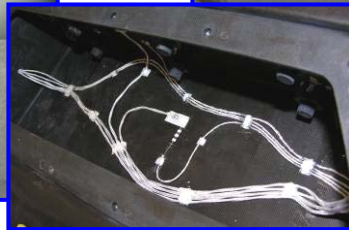
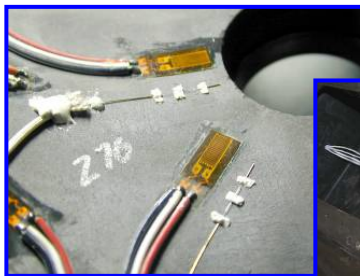
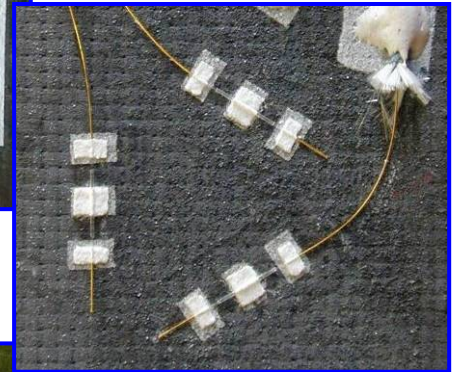
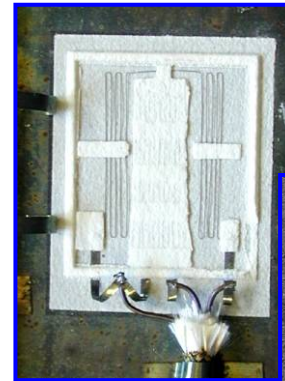
- Select sensor most suited to acquire needed information
- Develop sensor attachment techniques for structural material
- Validate strain and temperature measurements



Application and Sensor

Select sensor most suited to acquire needed information

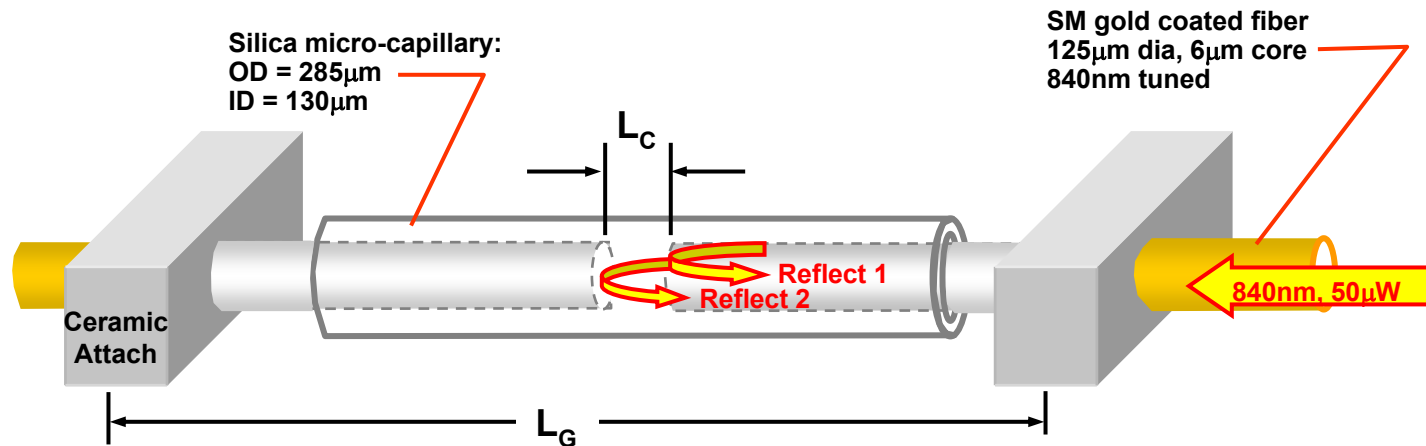
- Measurement required
- Substrate material
- Maximum test temperature
- Heating rate
- Static and / or dynamic environment



Application and Sensor

Static Strain Measurements

Extrinsic Fabry-Perot Interferometer (EFPI)



- Cavity Length (L_C): Distance (microns) separating the two reflecting fiber surfaces
- Gage Length (L_G): Sensitivity, distance (millimeters) separating the two points that attach the optical fiber to the substrate

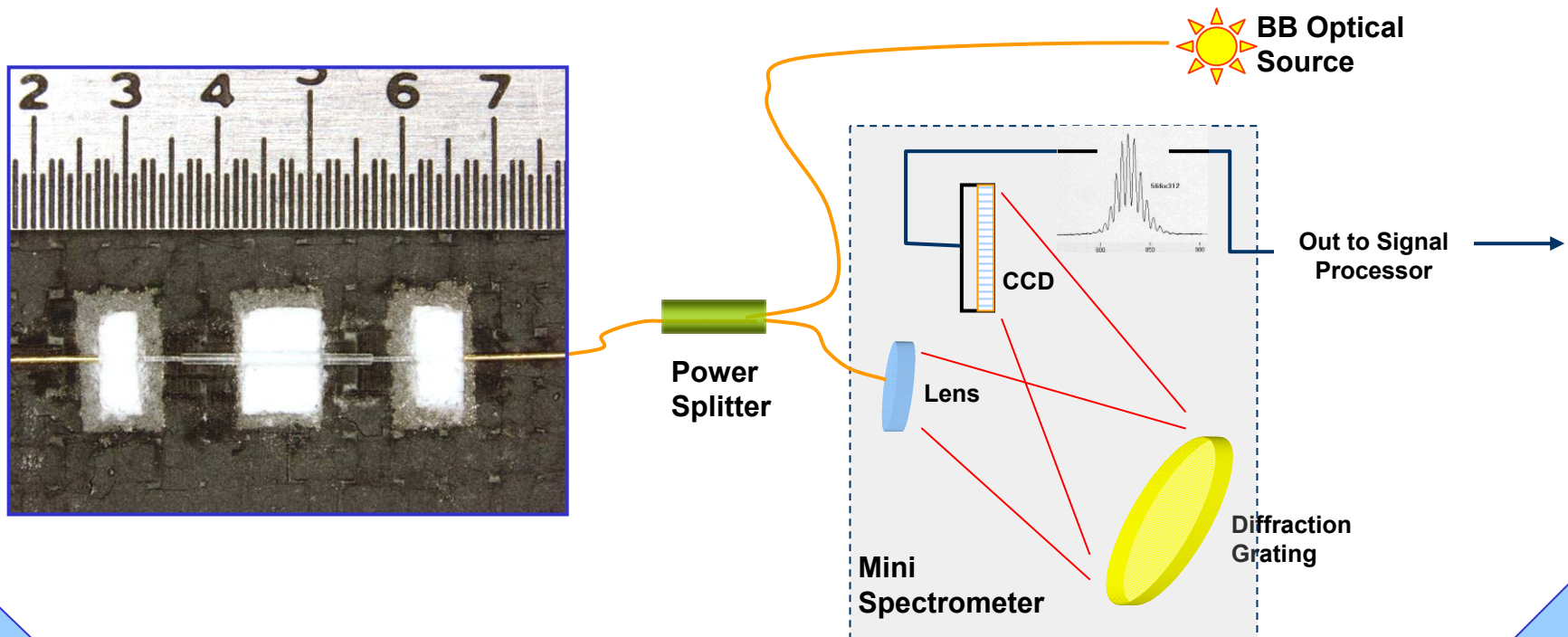
$$\text{Strain} = \Delta L_C / L_G \text{ (initial)}$$

$$\text{Apparent Strain } (\xi_{\text{app}}) = (\alpha_{\text{sub}} - \alpha_{\text{fiber}}) \Delta T$$

Application and Sensor

Static Strain Measurements

Single Mode Interferometer Signal Conditioning



Application and Sensor

Dynamic Strain Measurements

Electrical Resistive Strain Gage (SG)

Quarter-Bridge Strain Gage Typical Sensor Traits

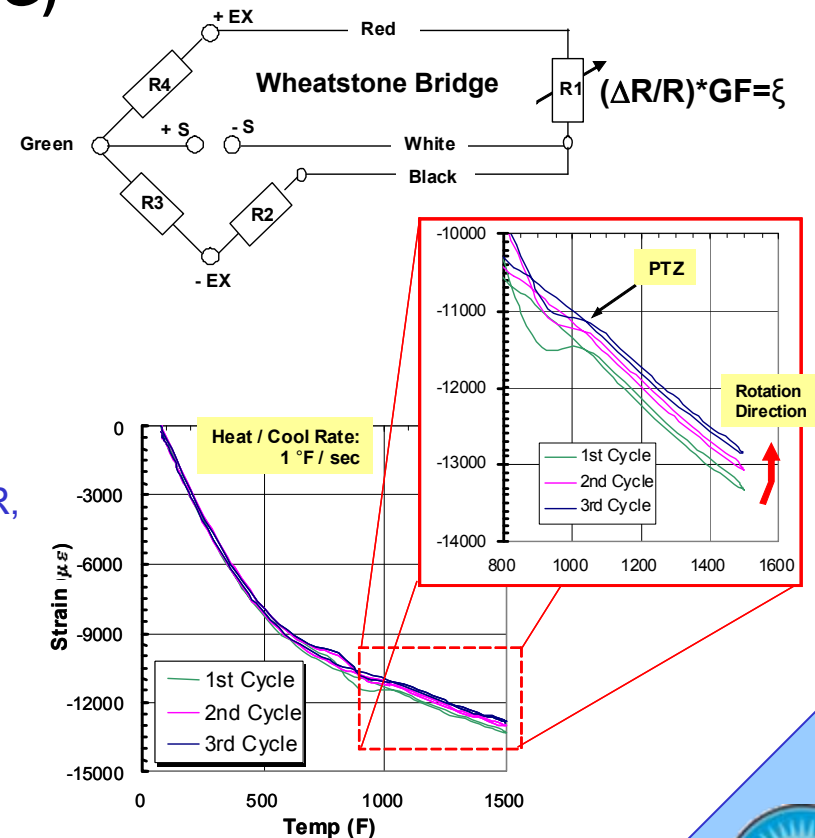
Pro's

- Sturdy / rugged thermal sprayed installation and spot-welded leadwire stakedown
- Available high sample rate DAS, usually AC coupled to negate large ξ_{app}

Con's

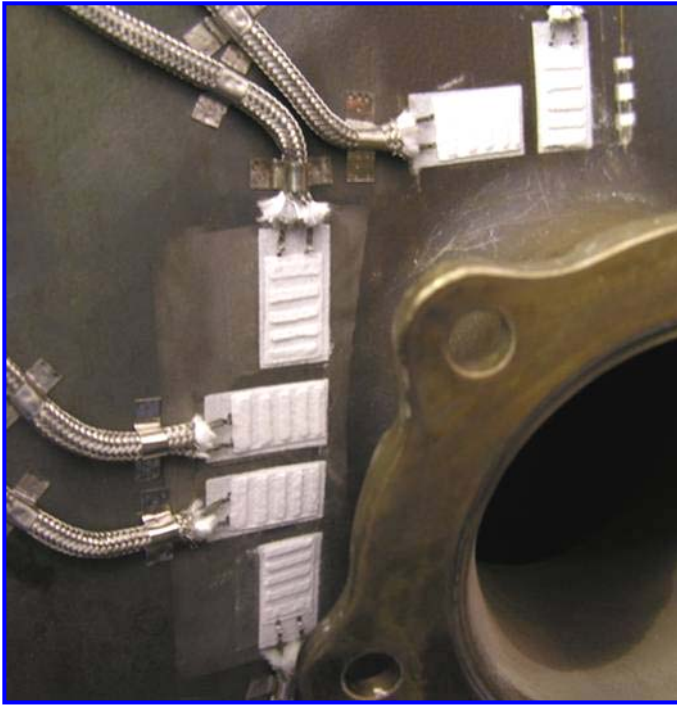
- Large magnitude ξ_{app} primarily due to wire TCR, slope rotates cycle-to-cycle
- Sensitivity (GF): Function of temperature

$$\xi_{app} = [TCR_{gage} / GF_{set} + (\alpha_{sub} - \alpha_{gage})] * (\Delta T)$$



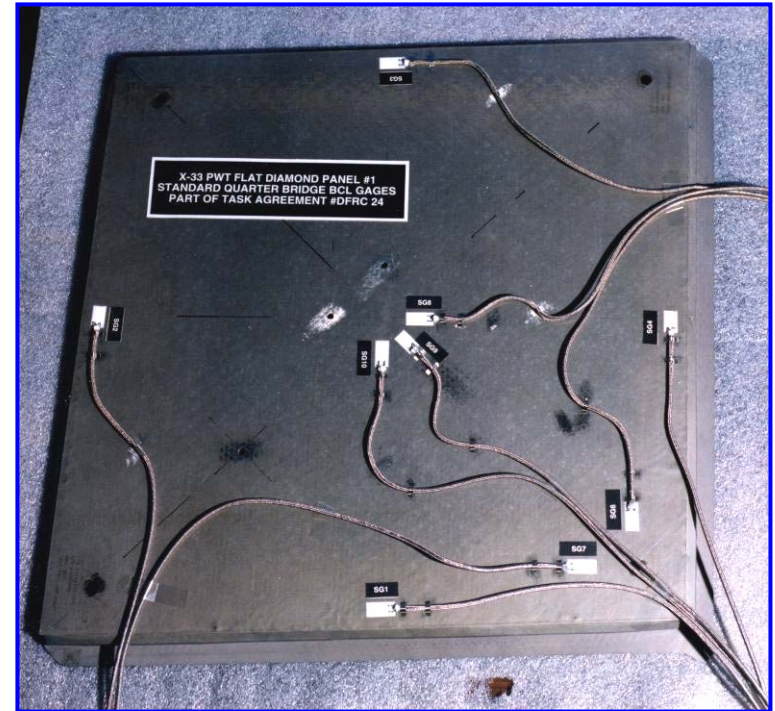
Application and Sensor

Dynamic Strain Measurement Examples



C-17 Engine Testing

- Test temperatures above 1100°F
- Engine intentionally unbalanced creating large peak-to-peak vibrations



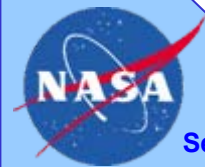
X-33 Sonic Fatigue Testing

- Dynamic loads as high as -158db
- Test temperatures above 1500°F
- High transient heating rates producing large thermal stresses

Attachment Techniques

Develop sensor attachment techniques for structural material

- Derive surface prep and optimal plasma spray parameters for applicable substrate
 - powder type, power level, traverse rate, and spraying distance
- Optimize / select cement that best fits application
- Improve methods of handling and protecting fragile sensors during harsh installation processes

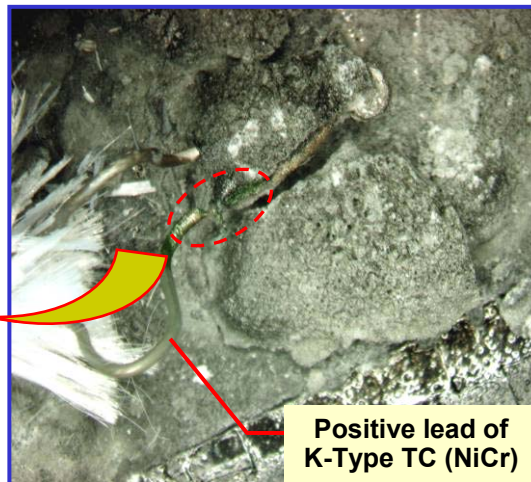


Attachment Techniques

Thermal Spray vs Cement

Thermal sprayed attachments are preferred even though cements are simpler to apply

- Cements are often corrosive to TC or strain gage alloys
 - Si / Pt, NaF / Fe-Cr-Al alloys, alkali silicate / Cr
- Cements are more prone to bond failure due to shrinkage and cracking caused when binders dissipate

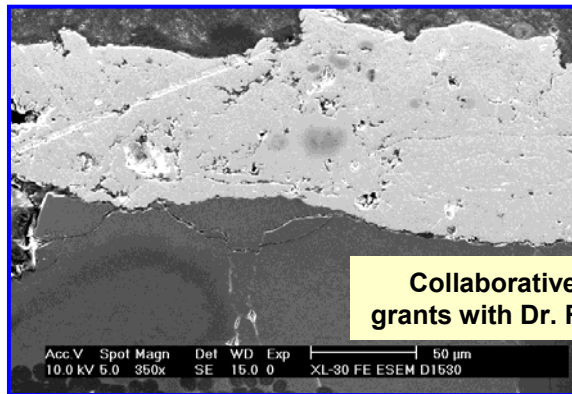


Attachment Techniques

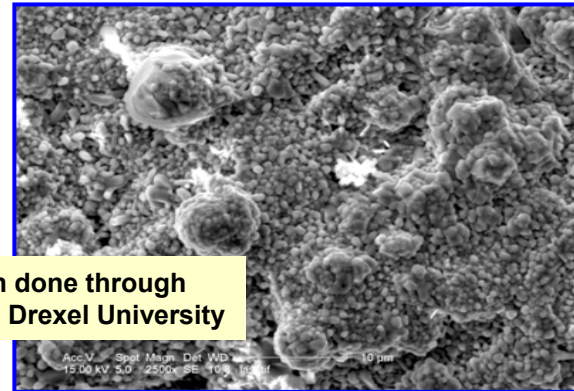
Thermal Spray Processes

Arc-plasma sprayed base coat

- Metallic Substrates: Used to transition high expansion substrate metal with low expansion sensor attachment material (Al_2O_3)
- CMC Substrates (inert testing): High melting-point ductile transitional metals (i.e. Ta, TiO_2 , & Mo) more conducive for attachment to smooth surfaces like SiC



Collaborative work has been done through grants with Dr. Richard Knight, Drexel University



Rokide flame-sprayed sensor attachment

- Applies a less dense form of alumina than plasma spraying
- Electrically insulates (encapsulate) wire resistive strain gages

Attachment Techniques

Thermal Spray Equipment

Thermal Spray Room

- 80KW Plasma System
- Rokide Flame-Spray System
- Powder Spray System
- Grit-Blast Cabinet
- Micro-Blast System
- Water Curtain Spray Booth

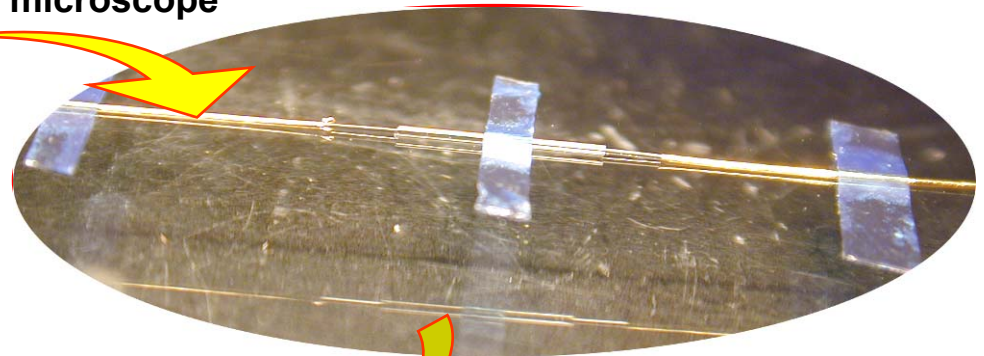


Attachment Techniques

Fiber Optic EFPI Installation

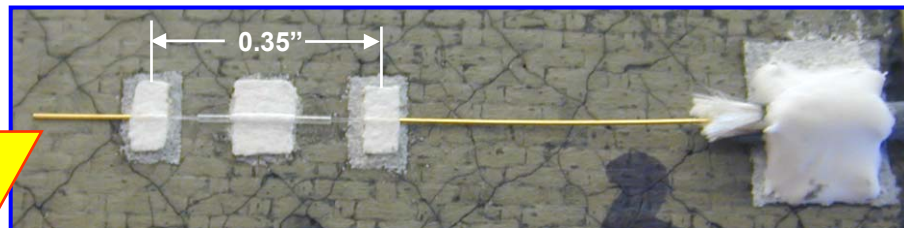


Fabricate sensor under microscope



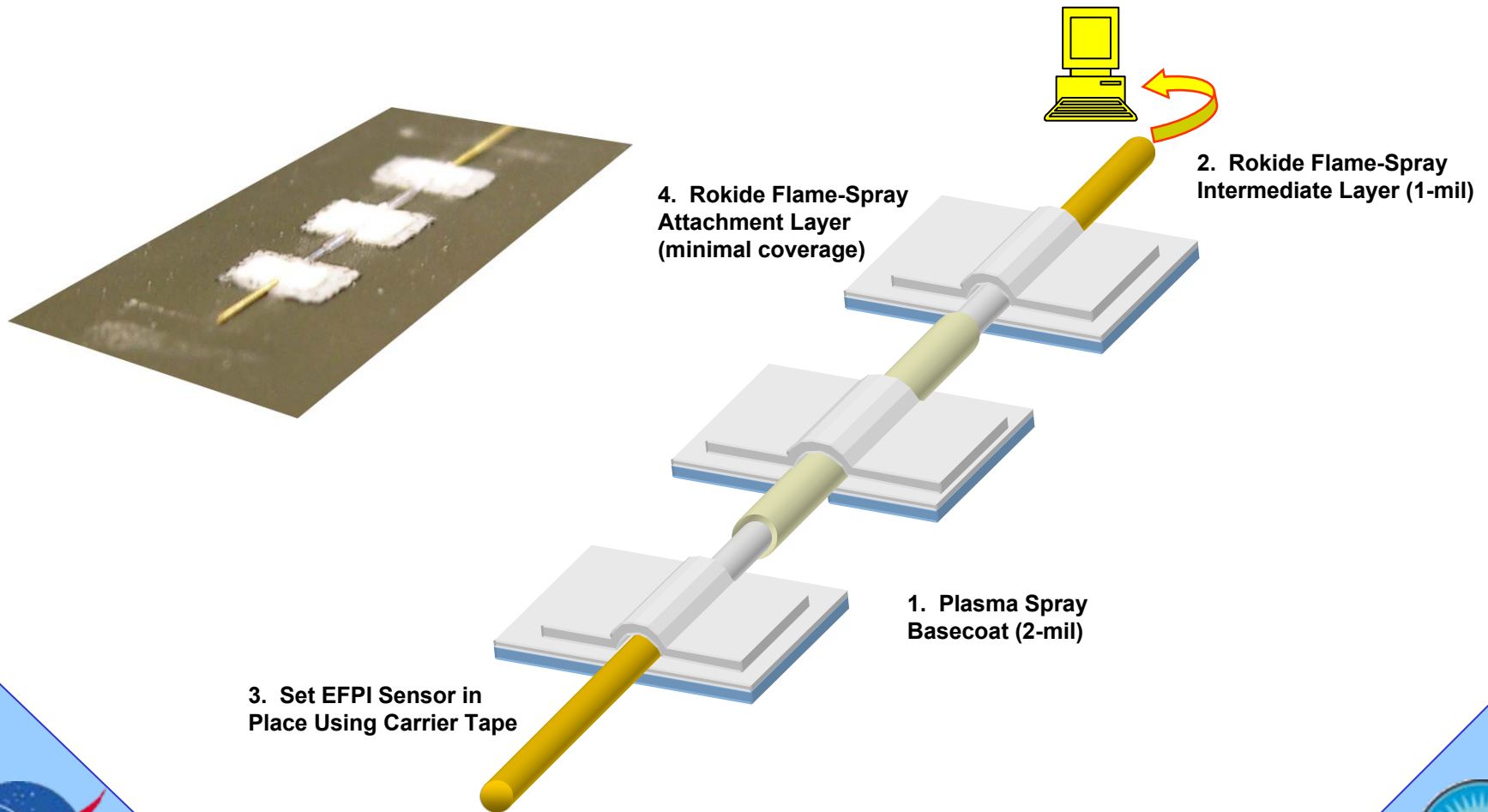
Transfer to thermal sprayed base coat using carrier tape

Flame-spray sensor attachment



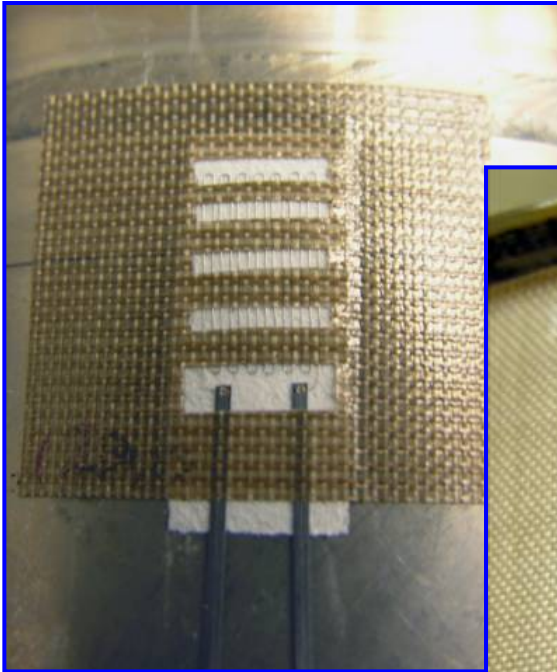
Attachment Techniques

Fiber Optic EFPI Installation



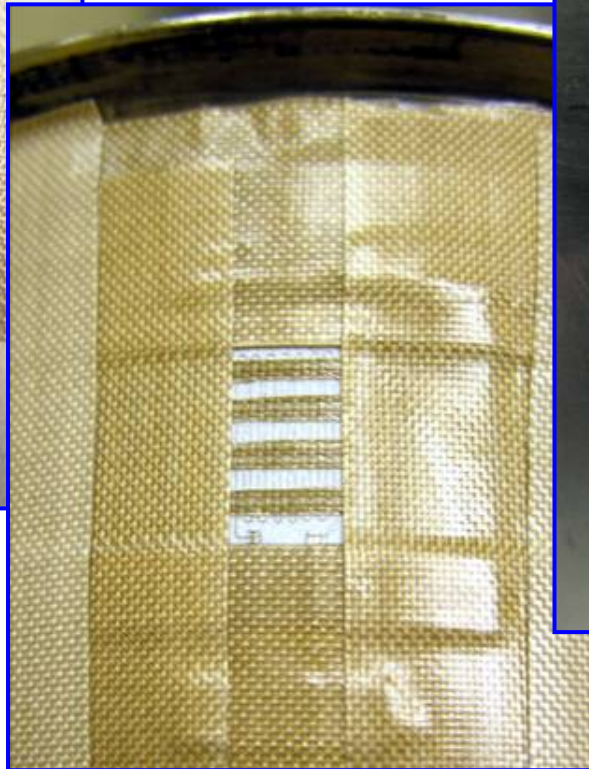
Attachment Techniques

Resistive Wire Strain Gage Installation



Place SG on thermal
sprayed basecoats
via carrier tape

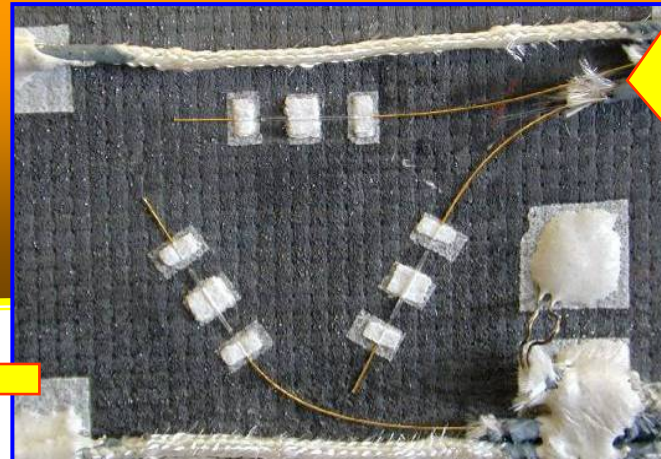
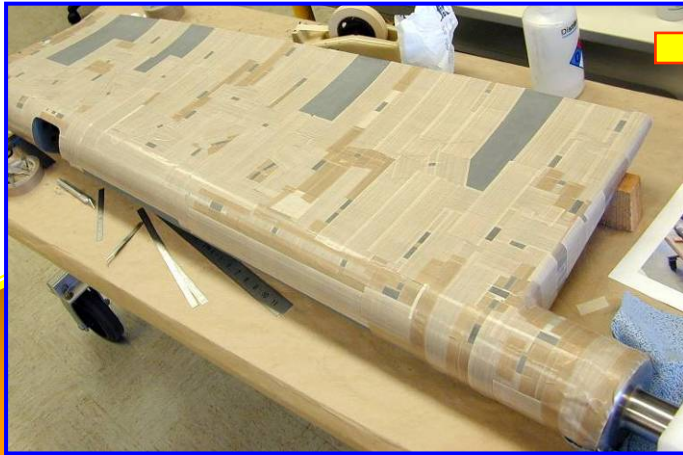
Apply flame-sprayed
tack and cover coats



Spot weld three-
conductor leadwire

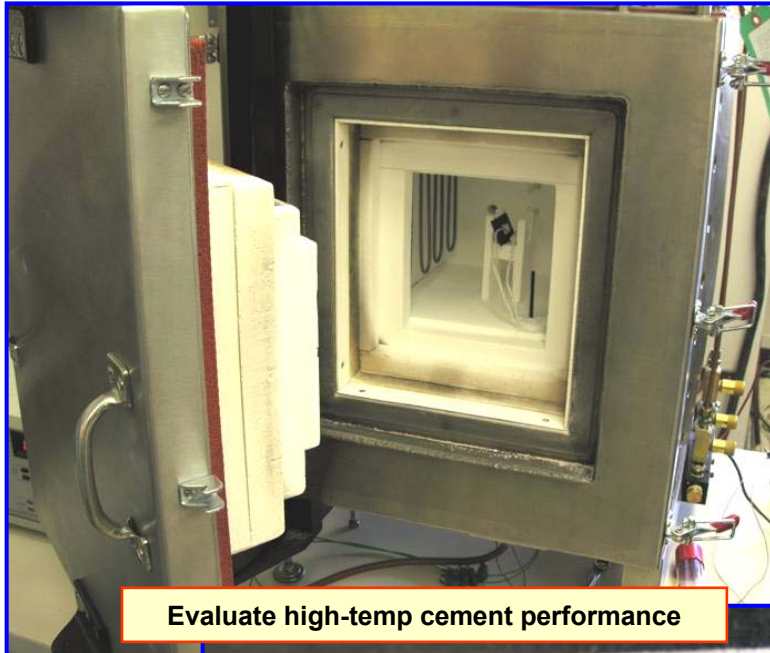
Attachment Techniques

Large-Scale Structures



Attachment Techniques

Thermocouple Junction

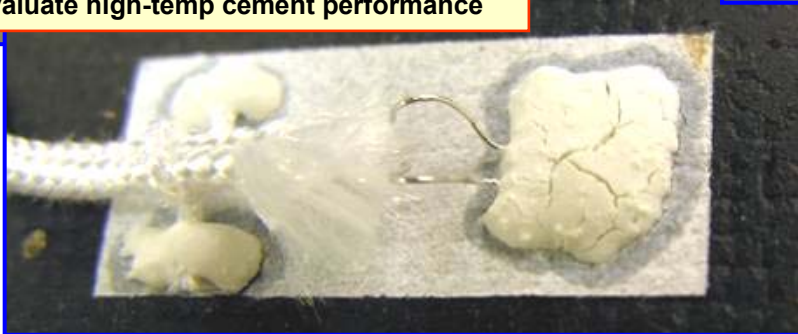


Rapid-Heat Furnace

- Air or inert (2600°F max)
- 8-in³ inner furnace with Molydisilicide elements



Thermal spray attachments must be as thin as possible to reduce sheering due to expansion differentials



Attachment Techniques

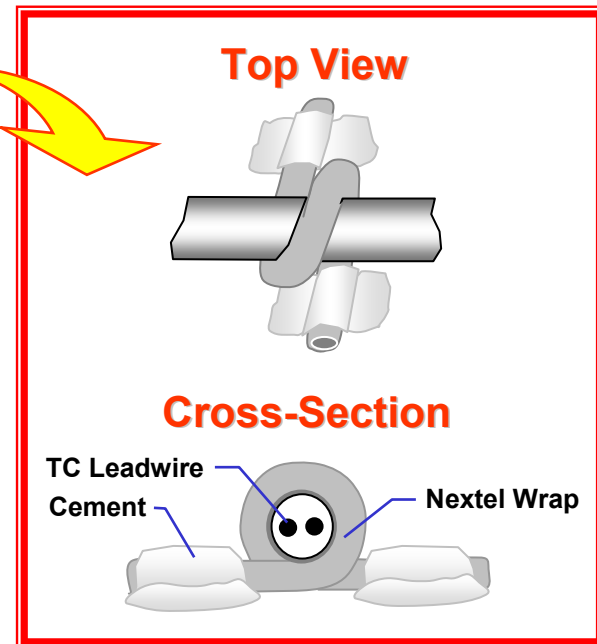
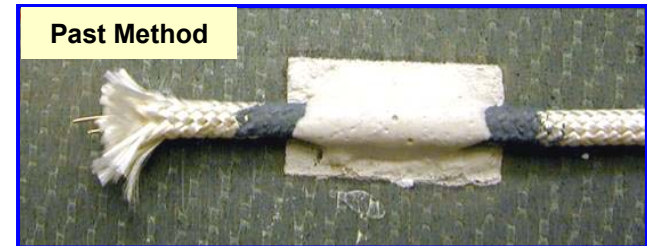
Thermocouple Leadwire

Improved Leadwire Stakedown

- Thermal sprayed base coats
- All Coverguard removed, only S-13 cement was used for TC attachment
- No cement applied directly on overbraid



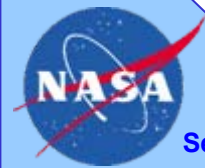
- Leadwires staked with tie-down method developed during National Aerospace Plane program
- Reshaped service loops to lay on basecoat surface



Evaluation / Characterization

Validate strain and temperature measurements

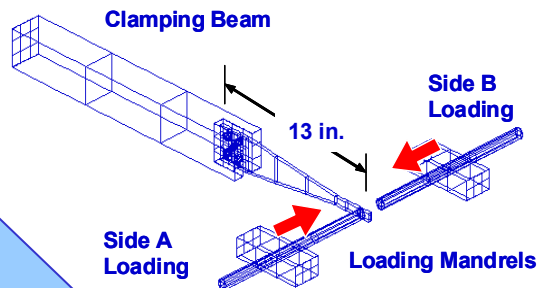
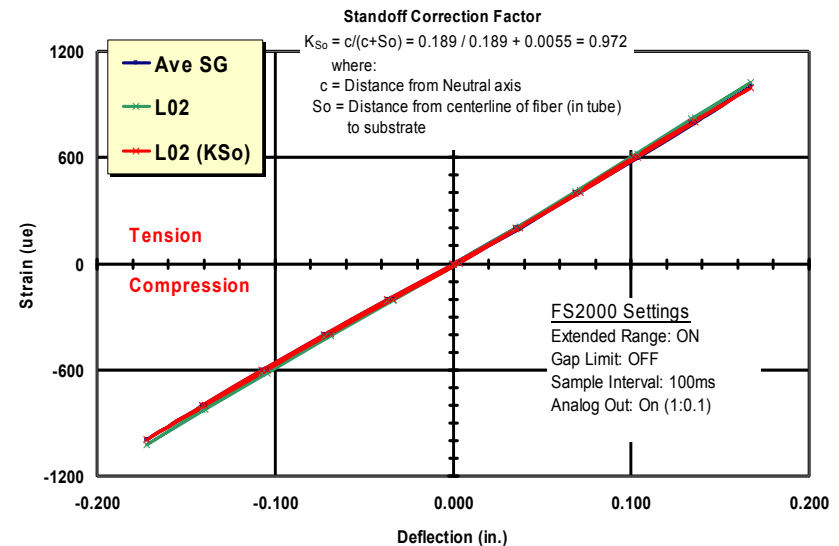
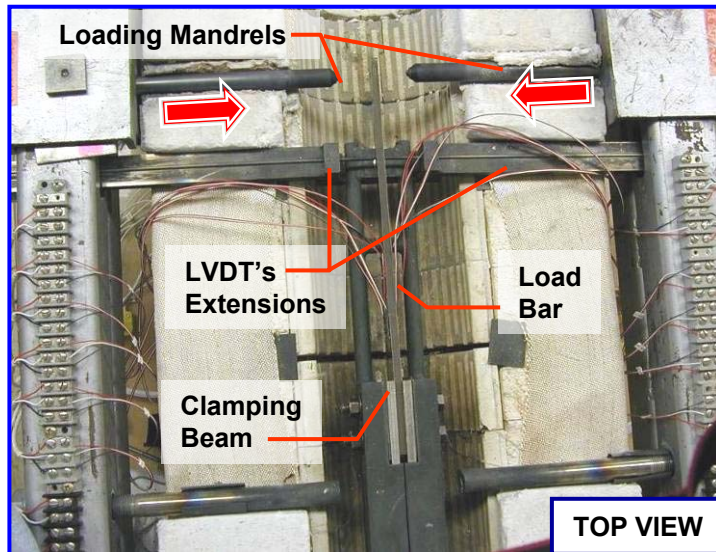
- Base-line / characterize high-temperature strain sensors on Inconel specimens
 - Known material spec's isolate substrate from inherent sensor traits prior to testing on more complex composites
- Evaluate / characterize sensitivity (GF) of strain sensors on ceramic composite substrates using laboratory combined thermal / mechanical load fixture
- Generate apparent strain curves for corrections
- Test and verify TC measurements in laboratory furnace under fast transient and steady-state conditions



Evaluation / Characterization

Combined Thermal / Mechanical Loading (Obsolete)

EFPI Combined Loading on IN625

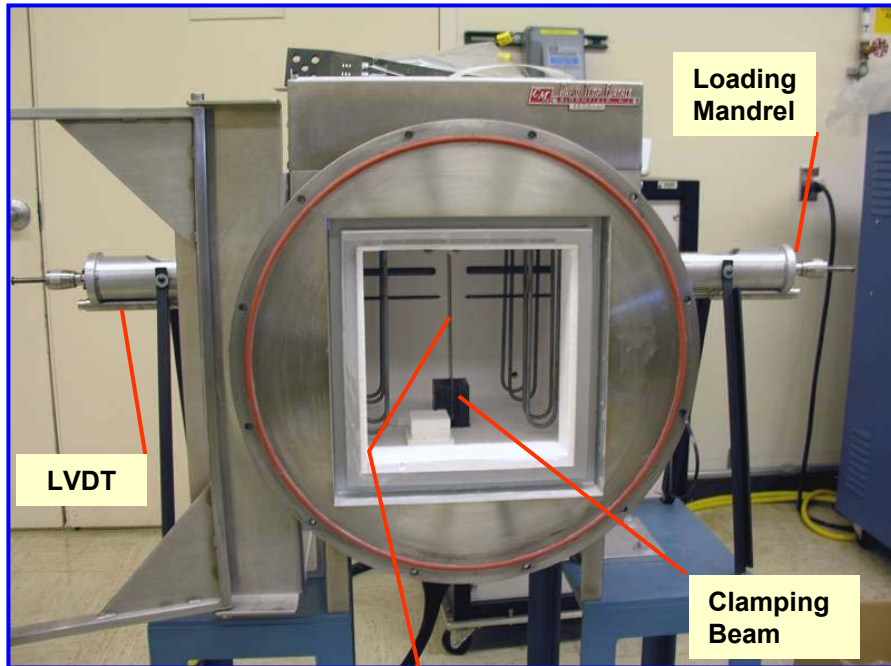


Thermal / Mechanical Cantilever Beam Testing of EFPI's

- Excellent correlation with SG to 550°F (3%)
- Very little change to 1200°F
- Slight drop in output slope above 1200°F
- Maximum gap readability uncertain at upper range temperatures on high expansion material

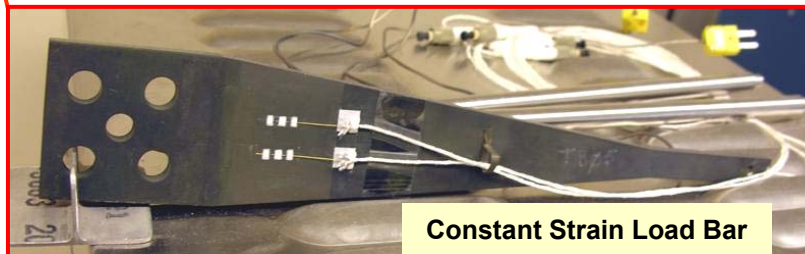
Evaluation / Characterization

Combined Thermal / Mechanical Loading (Current)



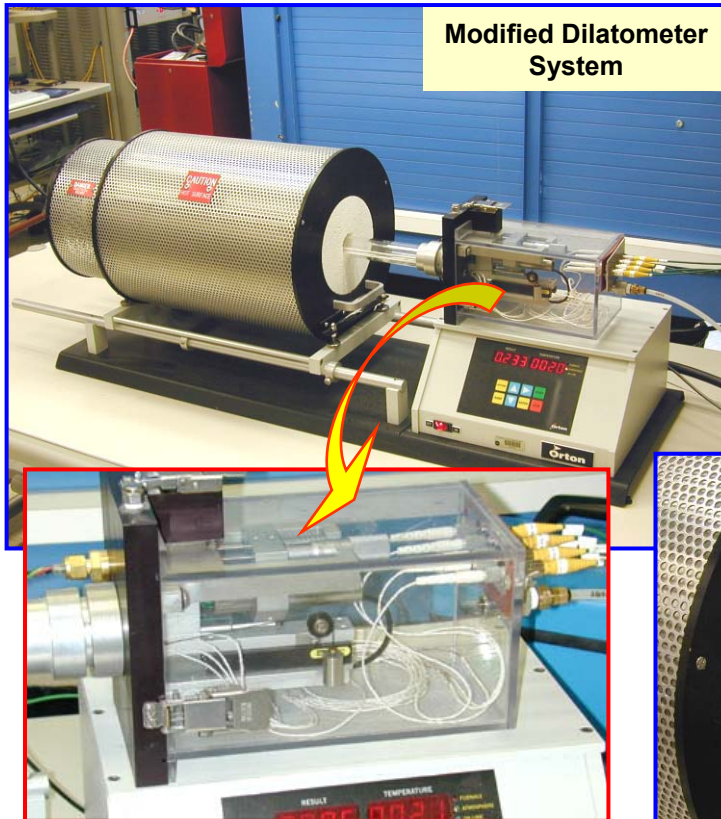
Furnace / cantilever beam loading system for sensitivity testing

- Air or inert (3000°F max)
- 12-in³ inner furnace with Molydisilicide elements
- Micrometer / mandrel side loading
- LVDT displacement measurements
- POCO Graphite hardware for inert environment testing of ceramic composites
- IN625 hardware for metallic testing in air
- Sapphire viewing windows



Evaluation / Characterization

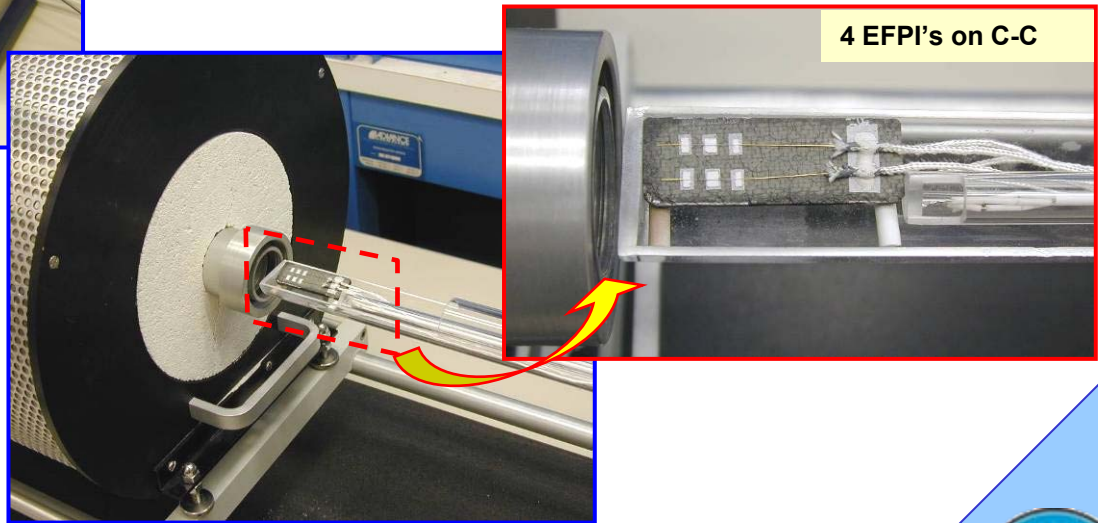
Dilatometer Testing



Sensor Characterization

Air or inert (3000°F max)

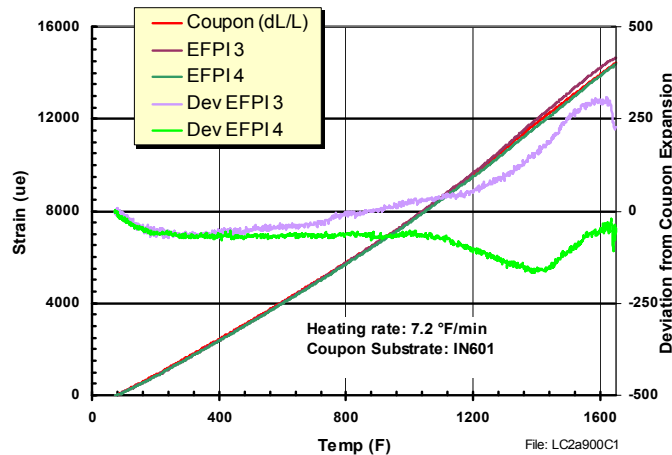
- Evaluate bond integrity
- Generate ξ_{app} correction curves
- Evaluate sensitivity and accuracy
- Evaluate sensor-to-sensor scatter, repeatability, hysteresis, and drift



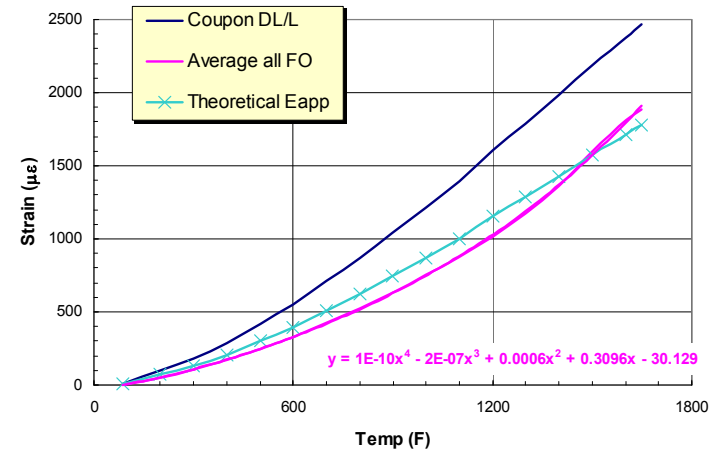
Evaluation / Characterization

EFPI Apparent Strain

Inconel Substrate



CMC Substrate



ξ_{app} Correction: The removal of inherent sensor traits and substrate expansion from indicated strain to acquire true applied strains or thermal stresses

$$\xi_{true} = \xi_{indicated} - \xi_{app}, \text{ where } \xi_{app} = (\alpha_{sub} - \alpha_{fiber}) * \Delta T$$

- Inconel (LH chart): Expansion ratio between IN and Si so large no sensor correction *required* (output primarily substrate expansion, $CTE * \Delta T$)
- CMC (RH chart): Small CTE ratio between C-SiC and Si requires a correction for the growth in fiber (lessening cavity gap) versus the expansion of the substrate
- Plots shows how well actual ξ_{app} curves followed theoretical

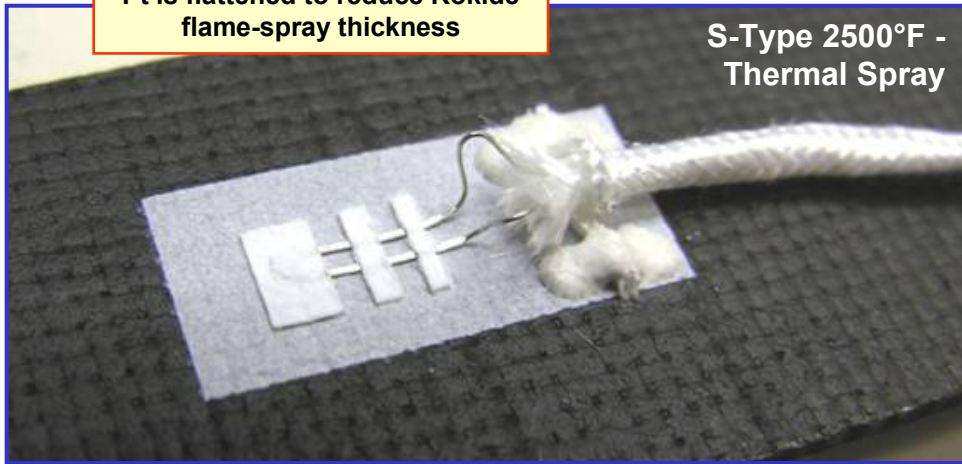


Evaluation / Characterization

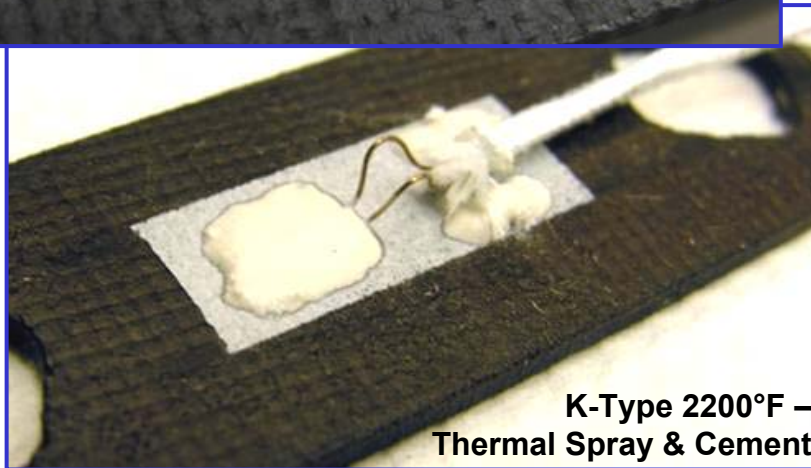
Current Ceramic Composite Temperature Measurements

Pt is flattened to reduce Rokide flame-spray thickness

S-Type 2500°F -
Thermal Spray



K-Type 2200°F –
Cement



K-Type 2200°F –
Thermal Spray & Cement

TC is isolated from high-strength
(but corrosive) SiC cement by a
benign (phosphate based) cement



Future Testing

- Test single-mode silica EFPI's in combined thermal / mechanical load fixture on C-C and C-SiC substrates
- Develop Sapphire strain sensor (multi-mode)
 - Keep precise parallel gap faces aligned throughout process
 - Develop precision transfer method (i.e. temporary alignment fixture)
 - Test in laboratory thermal / mechanical loads fixture to $> 2500^{\circ}\text{F}$
- Test and evaluate high-temperature fiber Bragg Gratings for use as strain and temperature sensors
- Develop accelerometer attachment method for high-temp GVT
- Attach and evaluate high-temperature heat flux gage
- Evaluate weldable (shim) EFPI strain sensor on Inconel
- Continue to improve reliable / rugged TC attachments to ceramic composites, including flight application

